

The Use of Coding and Diversity Combining for Mitigating Fading Effects in a DS/CDMA System

Pilar Díaz, *Member, IEEE*, and Ramón Agustí, *Member, IEEE*

Abstract—Spatial diversity is an attractive technology to cope with the fading channel encountered in mobile communications. This paper presents novel closed analytical expressions of the bit-error rate (BER) achievable in a coherent binary phase-shift-keying (CBPSK) direct-sequence code-division multiple-access (DS/CDMA) system for any power delay profile and for either postdetection selection or maximal ratio combining (MRC). In particular, expressions for the cutoff rate R_o and for its related parameter D are also formulated in order to assess the system performance under the consideration of some channel coding schemes. Finally, an exemplary study is carried out in order to illustrate the behavior of a realistic space-diversity code-division multiple-access (CDMA) system according to the analytical expressions that have been derived.

Index Terms—Channel coding, code-division multiple access, fading channel, mobile communications, spatial diversity.

I. INTRODUCTION

THE ADVANTAGES of using spatial diversity have been widely recognized in the code-division multiple-access (CDMA) field, although not much effort has been devoted so far in the open literature to assess analytically these techniques. In this paper, closed analytical expressions of the bit-error rate (BER) achievable with antenna diversity and ideal averaged power control are presented for a coherent binary phase-shift-keying (CBPSK) direct-sequence code-division multiple-access (DS/CDMA) system with a RAKE receiver in the presence of generic multipath Rayleigh fading. This might model rather well the CDMA system for high fading rates since, in practice, closed power control, as it is usually invoked in CDMA systems to mitigate the fast fading, loses effectiveness for high Doppler rates (f_m). Studies shown in [1] and [2] reveal that moderate f_m values only lead to moderate reductions on compensating the fast fading. That is, the fading statistics of the signal after closed power control remains nearly the same that those obtained with only averaged power control. In particular, for $f_m = 80$ Hz, as much as an 87% of the variability is maintained [1].

The analysis pursued in this work includes both *selection* and *maximal ratio combining* (MRC) of the outputs of P Rake

receivers corresponding to P different antennas. In particular, MRC is well suited as a form of microdiversity combining at the same site, while selection could be suited as a form of macrodiversity combining to be realized on the network side. In this case, every base station involved (usually, a total of two) receives the signal from one mobile. At a higher level in the network hierarchy, which belongs to the access network to the mobile interworking unit [3], only the base station with the best signal-to-interference ratio at the Rake output is selected. Moreover, the selection diversity performance allows us to have an analytical upper bound of the performance (in terms of BER) of the switching microdiversity scheme [4], [5]. This simple scheme uses P antennas, but only one RF front end and one Rake receiver, so that when the signal level at the output of the Rake crosses down a preestablished threshold, the input of the receiver is switched to another antenna.

No coding as well as convolutional channel coding schemes have also been considered. In the case of coding, closed expressions of the channel cutoff rate have been formulated in the presence of ideal interleaving (infinite depth), so that available bounds of the BER in terms of the channel cutoff rate R_0 can be used. In every case, as usually has been done in the related literature, the Gaussian model for interferences has been assumed.

The organization of this paper is as follows. Section III is devoted to assess BER expressions of a DS/CDMA system in the presence of Rayleigh fading under diversity combining. Both selection and MRC are considered as diversity schemes. In Section IV, the use of channel coding is also contemplated and the parameter D , which appears in the BER bounds for convolutional codes, is derived for soft decisions. Section V is devoted to analyze and compare the performance of both diversity schemes in conjunction with two different convolutional codes. Finally, in Section VI, some conclusions are drawn.

II. SYSTEM MODEL

CDMA is a digital multiple-access technique in which each subscriber has his own identification code and all the transmitted signals share the same frequency band of the spectrum. The identification code is an N -long pseudorandom binary sequence, unique for each active user. This sequence is made up of N waveforms, called chips, the duration of which is T_c . The code length expressed in time is T_b s, so $T_b = NT_c$.

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The authors are with the Department of Signal Theory and Communications, Universitat Politècnica de Catalunya, 08034 Barcelona, Spain (e-mail: pilar@xaloc.upc.es).

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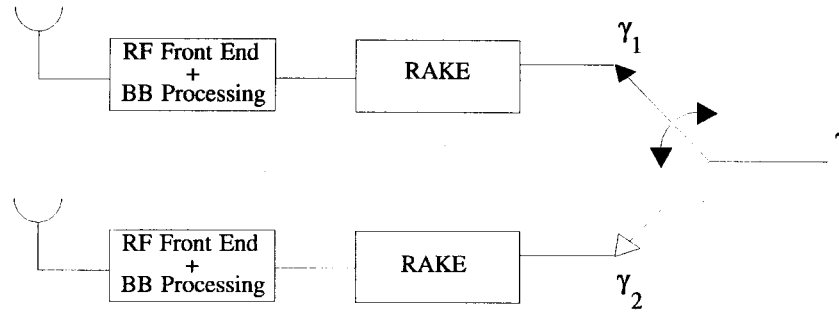


Fig. 1. Selection diversity of order 2 at reception.

The low-pass equivalent impulse response for the link between an active user and the base station is assumed to have L propagation paths

$$h(t) = \sum_{n=0}^{L-1} \alpha_n e^{j\theta_n} \delta(t - nT_c) \quad (1)$$

where the path amplitude α_n is assumed to be a Rayleigh random variable and the path phase θ_n a uniform random variable within $[0, 2\pi]$.

The optimum receiver of a DS/CDMA system operating in such a kind of environments, called the Rake receiver [6], has also been considered in order to take advantage of the multipath propagation, characteristic in mobile communications. This receiver recovers the information carried by any propagation path since it has available L -transmitted signal replicas. However, when the number of propagation paths L is so large that the receiver complexity increases excessively, or when the signal power received via the last replicas is negligible with regard to that of the first ones, the Rake receiver only combines the received signals from M (out of L) different propagation paths.

Furthermore, the presence of deep fades, characteristic in Rayleigh fading channels, produce high error rates. To counteract the effects of these propagation conditions, one may resort to employ antenna diversity in conjunction with the multipath diversity provided by the Rake receiver.

III. BIT-ERROR PROBABILITY UNDER DIVERSITY COMBINING

Closed expressions of the bit error probability have been derived for a coherent BPSK DS/CDMA system under Rayleigh multipath fading when P antennas are employed at the receiver. Selection diversity and MRC have been considered and compared as different form of diversity.

1) *Selection Diversity*: Fig. 1 shows the receiver structure for the particular case of selection diversity with two antennas at reception. The receiver contains the RF front end, a baseband processing module, and the Rake combiner after the output of each antenna.

γ_i denotes the overall signal-to-interference ratio at the output of the Rake corresponding to the i th antenna and is given by [6]

$$\gamma_i = \sum_{k=0}^{M-1} \gamma_{ki} \quad (2)$$

where M is the number of arms in the Rake and γ_{ki} ($i = 1, \dots, P$) is the signal-to-interference ratio of the k th path in the i th antenna. When selection is employed as form of diversity, the signal-to-interference ratio γ before decision is given by

$$\gamma = \max(\gamma_1, \dots, \gamma_P). \quad (3)$$

For coherent BPSK signaling, the averaged BER can be expressed as

$$P_e = E\left[\frac{1}{2} \operatorname{erfc}(\sqrt{\gamma})\right]. \quad (4)$$

In order to assess the expression of P_e , the probability density function (pdf) of γ must be determined. It can be obtained from the pdf of $\gamma_1, \dots, \gamma_P$, which are given by [6]

$$f_{\gamma_i} = \sum_{k=0}^{M-1} \frac{\pi_{ki}}{\bar{\gamma}_{ki}} \exp\left(-\frac{\gamma_i}{\bar{\gamma}_{ki}}\right), \quad i = 1, \dots, P \quad (5)$$

in the presence of different Rayleigh fading. $\bar{\gamma}_{ki}$ is the signal-to-interference ratio of every path, and the coefficients in the above expression π_{ki} can be expressed as

$$\pi_{ki} = \prod_{\substack{j=0 \\ j \neq k}}^{M-1} \frac{\bar{\gamma}_{ki}}{\bar{\gamma}_{ki} - \bar{\gamma}_{ji}}, \quad i = 1, \dots, P. \quad (6)$$

Therefore, the pdf of γ can be expressed as

$$\begin{aligned} f_{\gamma}(\gamma) &= \sum_{i=1}^P F_{\gamma_i}(\gamma) f_{\gamma_i}(\gamma) \\ &= \sum_{i=1}^P \sum_{n=0}^{M-1} \pi_{ni} \left[1 - \exp\left(-\frac{\gamma}{\bar{\gamma}_{ni}}\right) \right] \\ &\quad \cdot \sum_{k=0}^{M-1} \frac{\pi_{ki}}{\bar{\gamma}_{ni}} \exp\left(-\frac{\gamma}{\bar{\gamma}_{ni}}\right) \end{aligned} \quad (7)$$

where $F_x(x)$ represents the distribution function of the random variable x . From the expression of the pdf of γ , it is possible to compute the mean BER given by (4) for coherent BPSK and Rayleigh fading with antenna diversity. The expression for the BER, which has been derived in detail in Appendix

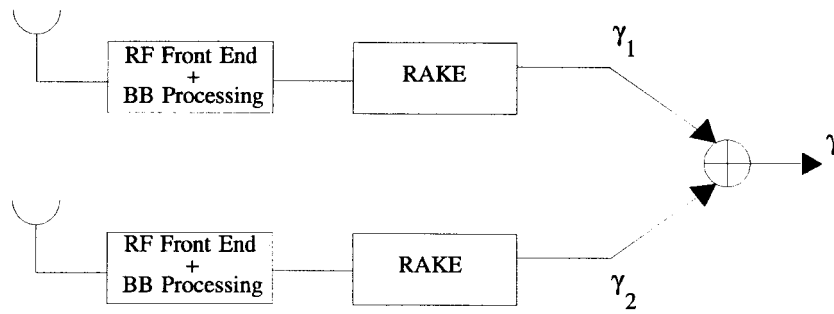


Fig. 2. MRC diversity of two at reception.

A, is as follows:

$$P_e = \frac{1}{2} \sum_{i=1}^P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_{ni} \pi_{ki} \cdot \left[\frac{\bar{\gamma}_{ki}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni}} + \frac{\bar{\gamma}_{n1}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni}} \right] \cdot \left[\sqrt{\frac{\bar{\gamma}_{ki} \bar{\gamma}_{ni}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni} + \bar{\gamma}_{ki} \bar{\gamma}_{ni}}} - \sqrt{\frac{\bar{\gamma}_{ki}}{1 + \bar{\gamma}_{ki}}} \right]. \quad (8)$$

2) *MRC Diversity*: Fig. 2 shows the receiver structure for the particular case of MRC diversity with two antennas at reception, analogously to Fig. 1 for selection diversity.

When MRC is employed as form of diversity, γ before decision can be expressed as

$$\gamma = \sum_{i=1}^P \gamma_i = \sum_{i=1}^P \sum_{k=0}^{M-1} \gamma_{ki} \quad (9)$$

where γ_i is again given by (2).

The expression of the mean BER is (4) for coherent BPSK signaling, so the pdf of γ must be determined in order to assess P_e . It can be done by means of its characteristic function, which can be expressed as

$$\psi_\gamma = \prod_{k=0}^{M-1} \prod_{i=1}^P \frac{1}{1 - j\omega \bar{\gamma}_{ki}} \quad (10)$$

since the random variables γ_{ki} ($i = 1, \dots, P$ and $k = 0, \dots, M-1$) are statistically independent. Therefore, the pdf of γ is determined from the inverse Fourier transform of ψ_γ given by

$$f_\gamma(\gamma) = \sum_{k=0}^{M-1} \sum_{i=1}^P \frac{\pi_{ki}}{\bar{\gamma}_{ki}} \exp\left(-\frac{\gamma}{\bar{\gamma}_{ki}}\right) \quad (11)$$

provided that $\bar{\gamma}_{ki}$ have different values. The parameters π_{ki} are given by (6). In such a case, the expression of the mean BER in presence of Rayleigh fading can be directly derived from [6]

$$P_e = \frac{1}{2} \sum_{k=0}^{M-1} \sum_{i=1}^P \pi_{ki} \left[1 - \sqrt{\frac{\bar{\gamma}_{ki}}{1 + \bar{\gamma}_{ki}}} \right]. \quad (12)$$

When $\bar{\gamma}_{k1} = \bar{\gamma}_{k2} = \dots = \bar{\gamma}_{kP}$ ($k = 0, \dots, M-1$), the above expression for the mean BER is no longer valid, and in this case, the characteristic function is expressed as

$$\psi_\gamma = \prod_{k=0}^{M-1} \frac{1}{(1 - j\omega \bar{\gamma}_{k1})^P}. \quad (13)$$

Only for $P = 2$ it is possible to derive a simple and closed analytical expression for the pdf of variable γ , which is computed as the inverse Fourier transform of ψ_γ and given by

$$f_\gamma(\gamma) = \sum_{k=0}^{M-1} \pi_{k1} \left[\frac{\gamma}{\bar{\gamma}_{k1}^2} - \frac{2}{\bar{\gamma}_{k1}} \sum_{j \neq k} \frac{\bar{\gamma}_{j1}}{\bar{\gamma}_{k1} - \bar{\gamma}_{j1}} \right] \cdot \exp\left(-\frac{\gamma}{\bar{\gamma}_{k1}}\right). \quad (14)$$

From (14), it is possible to determine again the mean BER for coherent BPSK with Rayleigh fading and antenna MRC diversity. The expression of the mean BER, which has been derived in detail in Appendix B, is as follows:

$$P_e = \sum_{k=0}^{M-1} \pi_{k1} \left[\left(\frac{1 - \mu_{k1}}{2} \right)^2 (2 + \mu_{k1}) - (1 - \mu_{k1}) \sum_{j \neq k} \frac{\bar{\gamma}_{j1}}{\bar{\gamma}_{k1} - \bar{\gamma}_{j1}} \right] \quad (15)$$

where

$$\mu_{k1} = \sqrt{\frac{\bar{\gamma}_{k1}}{1 + \bar{\gamma}_{k1}}}. \quad (16)$$

IV. CODING WITH SOFT DECISIONS

In mobile radio communication systems, there exists the need to employ forward-error-correction (FEC) techniques in order to protect the information against the severity of the multipath propagation. Moreover, it is well known that in spread-spectrum systems, as CDMA systems are, the use of channel coding does not require additional allocation of bandwidth [7]. In case of using convolutional codes as well as decoders that work with soft decisions at their inputs, bounds on the BER may be obtained by resorting to the expression [8]

$$P(b) \leq G(D) \quad (17)$$

where $G(\cdot)$ is a function determined solely by the specific code, whereas the parameter D depends only on the coding channel and the decoder metric.

The use of this bound causes the parameter- D appearance, which is related to the cutoff rate R_o as follows [8]:

$$D = 2^{-R_o+1} - 1 \quad (18)$$

and is defined as

$$D = \min_{\lambda \geq 0} D(\lambda) \quad (19)$$

where

$$D(\lambda) = E[e^{\lambda r(x^* - x)} | x]. \quad (20)$$

In the above expression, x and x^* represent two different encoded sequences, and r is the received sequence when x has been the transmitted one. The parameter D does not depend on the code, but on the channel, modulation scheme, receiver, and also on the kind of decisions employed by the decoder, that is, hard or soft decisions. Therefore, in order to assess the BER as a function of the capacity, it is necessary to derive the expression of the parameter D as shown below.

When the decoder works with hard decisions, D depends directly on the BER of the channel, and is given by [9]

$$D = \sqrt{4P_e(1 - P_e)} \quad (21)$$

where P_e is the average BER at the decoder input.

When it works with soft decisions, D depends on the channel statistics and transmission schemes. In particular, when selection diversity with P antennas having the same signal-to-interference ratio for paths with identical delays is employed in a Rayleigh multipath channel, the expression of D for coherent BPSK, which has been given in detail in Appendix C, is as follows:

$$D = P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_{n1} \pi_{k1} \cdot \left[\frac{1}{1 + \bar{\gamma}_{k1}} - \frac{\bar{\gamma}_{n1}}{\bar{\gamma}_{n1} + \bar{\gamma}_{k1} + \bar{\gamma}_{n1} \bar{\gamma}_{k1}} \right] \quad (22)$$

where π_{n1} and π_{k1} are given by (6). On the other hand, when MRC is selected as form of diversity, the parameter D can be expressed as (see Appendix D)

$$D = \prod_{n=0}^{M-1} \left(\frac{1}{1 + \bar{\gamma}_{n1}} \right)^2. \quad (23)$$

V. SYSTEM PERFORMANCE

In order to illustrate the behavior of a space-diversity-based CDMA system according to the expressions obtained above and show how to assess the performance of such a system in a given environment, we have first computed from (8) and (15) the mean BER of a two-antenna diversity DS/CDMA cellular system in a Rayleigh multipath environment with the same statistics in both antennas.

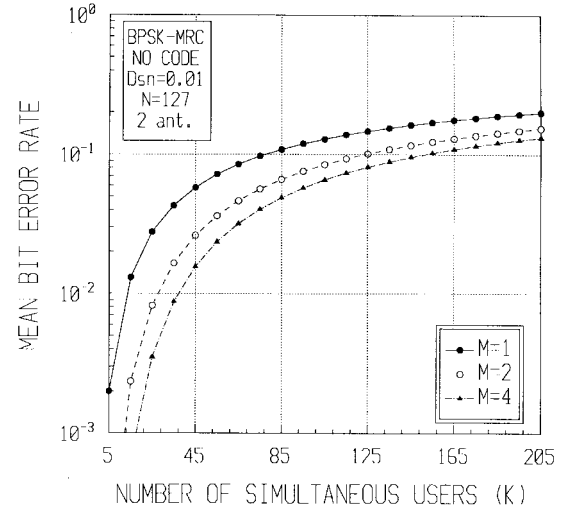


Fig. 3. Mean BER for selection diversity with two antennas at the receiver.

To compare the different diversity combining schemes, let us assume the power delay profile (PDP) of the channel $p(\tau)$ to be exponential [11] and identical for any antenna

$$p(\tau) = \frac{1}{D_s} \exp\left(-\frac{\tau}{D_s}\right) \quad (24)$$

where D_s denotes the delay spread of the channel. In this situation, the variance of α_{ki} , which represents the complex Gaussian amplitude of the k th propagation path between the transmitter and the i th antenna at reception, is given by

$$\bar{\alpha}_{ki}^2 = p(kT_c) \quad (25)$$

where T_c is the chip interval.

The mean signal-to-interference ratio of the k th path at the i th antenna can be formulated as [10]

$$\bar{\gamma}_{ki} = \frac{\bar{\alpha}_{ki}^2}{\frac{2\rho K}{3N} \sum_{j=0}^{L-1} \bar{\alpha}_{ji}^2} \quad (26)$$

where K is the number of simultaneous users of the system within the cell of interest, ρ is the reuse factor that takes into account interference from other cells, N is spread-spectrum processing gain, and L the total number of arrival paths at the receiver.

Furthermore, in order to assess the performance of the system for different levels of complexity in the Rake receiver, which is actually built up with M arms, we have assumed representative values for the parameters on the expressions derived for the mean BER, as shown below:

- 1) delay spread normalized to the bit period T_b : $D_{sn} = D_s/T_b = 0.01$;
- 2) processing gain: $N = 127$;
- 3) reuse factor [12]: $\rho = 1.7$.

Figs. 3 and 4 show the mean BER for coherent BPSK of a DS/CDMA cellular system that make use of two antennas at reception with selection and MRC diversity, respectively, and in particular, for the environment described above.

TABLE I
BE OF A DS/CDMA SYSTEM WITH CBPSK AND CHANNEL CODING (r -1/3 CONVOLUTIONAL CODE AND HARD DECISIONS)

M	No Diversity	Selection Div.	MRC Diversity
1	0.07	0.16	0.21
2	0.15	0.25	0.38
4	0.21	0.31	0.49

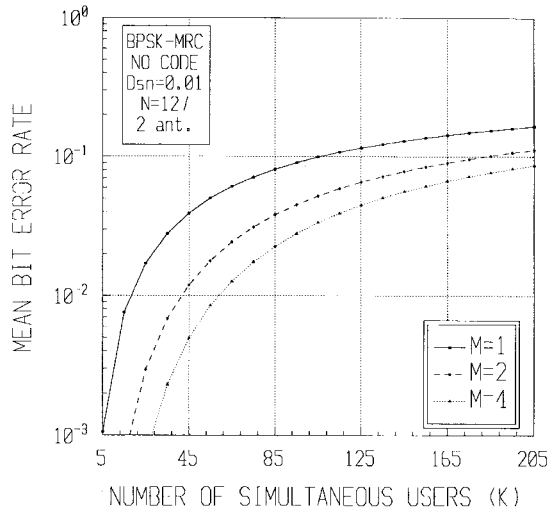


Fig. 4. Mean BER for MRC diversity with two antennas at the receiver.

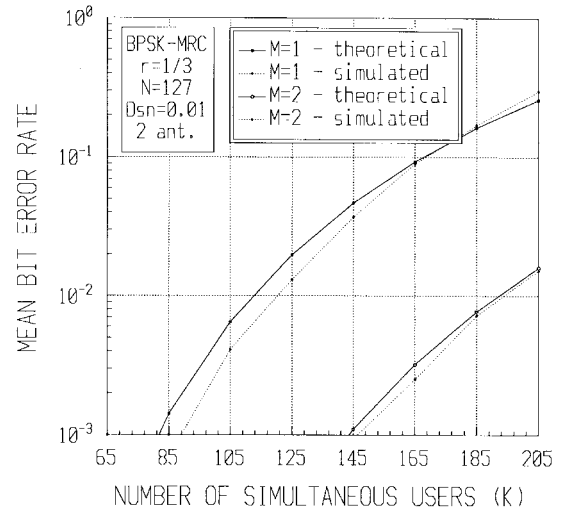


Fig. 5. Mean BER for MRC diversity with a r -1/3 convolutional code.

Concerning channel coding, two representative convolutional codes have been considered. Bounds on the mean BER for each one of them, derived from the Chernoff bound, are given by [9].

- 1) r -1/2 convolutional code with generator polynomial 133 171 (octal)

$$P_b \leq \frac{1}{2} (36D^{10} + 211D^{12} + 1404D^{14} + 11633D^{16}) \quad (27)$$

- 2) r -1/3 convolutional code with generator polynomial 133 145 175 (octal)

$$P_b \leq \frac{1}{2} (7D^{15} + 8D^{16} + 22D^{17} + 44D^{18}). \quad (28)$$

In order to compare the different schemes, the system performance has been evaluated in terms of the bandwidth efficiency, which is defined as the number of bits simultaneously transmitted by K users divided by the total available bandwidth and which is given by [10]

$$BE = \frac{Kr}{N} \quad (29)$$

where r is the coding rate.

To assess the preciseness of the analytical results obtained from the derived expressions of the mean BER, they have been compared with results obtained from simulations. To do that, an identical channel to that assumed to derive the analytical expressions has been simulated, ideal averaged power control has been assumed and the r -1/3 convolutional code has been taken as representative. The encoder and decoder of the

convolutional code have also been simulated in order not only to evaluate the preciseness of the obtained analytical expressions, but also the bounds given in (27) and (28). The theoretical results and those obtained in the simulations are depicted in Fig. 5. The curves shown in this figure are so close for both $M = 1$ and $M = 2$ that it can be stated that the upper bounds on the mean BER for convolutional codes are very tight, except when the channel introduces too many errors ($P_b > 10^{-1}$) so that the convolutional decoder significantly degrades and bounds on the BER are no longer valid. Moreover, when M increases the bounds on the BER tend to be tighter as it is expected.

Table I shows the BE for a DS/CDMA cellular system with no diversity (only one antenna), selection diversity, and MRC diversity (two antennas). It has been computed for the value of K that supports a transmission with a mean BER = 10^{-3} . In this case, the r -1/3 convolutional code with hard decisions has been considered as the channel coding employed in the system. In examining the BE values shown in Table I, it is apparent that diversity significantly improves capacity.

Table II shows the BE for a DS/CDMA system with selection diversity for both convolutional codes ($r = 1/2$ and $r = 1/3$) with hard and soft decisions and Table III for MRC diversity. In both cases, selection or MRC, the BE is nearly twice greater when the decoder works with soft decisions, and as a result, the capacity may be increased in the same way.

In all the tables shown above, it can also be noticed the capacity gain in terms of receiver complexity by means of the parameter M .

TABLE II
BE OF A DS/CDMA SYSTEM WITH CBPSK AND CHANNEL CODING FOR SELECTION DIVERSITY

M	r=1/2 hard	r=1/2 soft	r=1/3 hard	r=1/3 soft
1	0.10	0.252	0.16	0.328
2	0.19	0.382	0.25	0.475
4	0.25	0.469	0.31	0.564

TABLE III
BE OF A DS/CDMA SYSTEM WITH CBPSK AND CHANNEL CODING FOR MRC DIVERSITY

M	r=1/2 hard	r=1/2 soft	r=1/3 hard	r=1/3 soft
1	0.14	0.346	0.21	0.449
2	0.29	0.567	0.38	0.693
4	0.39	0.716	0.49	0.858

VI. CONCLUSIONS

In summary, novel closed analytical expressions have been derived for the mean BER of a p -antenna postdetection selection diversity and MRC diversity DS/CDMA cellular system under an ideal averaged power control scheme and under any generic Rayleigh multipath environment. It has also been obtained tight upper bounds on the BER in terms of the cutoff rate for such diversity schemes when convolutional codes and soft decisions are employed. These expressions, the preciseness of which has been evaluated through simulations, have allowed us to assess the system performance and compare the gain in capacity for any of the analyzed schemes in the presence of a realistic environment.

APPENDIX A

To simplify the computation of

$$P_e = \frac{1}{2} E[\text{erfc}(\sqrt{\gamma})] \\ = \frac{1}{2} \int_0^\infty \text{erfc}(\sqrt{\gamma}) \sum_{i=1}^P \sum_{n=0}^{M-1} \pi_{ni} \left[1 - \exp\left(-\frac{\gamma}{\bar{\gamma}_{ni}}\right) \right] \\ \cdot \sum_{k=0}^{M-1} \frac{\pi_{ki}}{\bar{\gamma}_{ki}} \exp\left(-\frac{\gamma}{\bar{\gamma}_{ki}}\right) d\gamma \quad (30)$$

let us make the change of variable $x = \sqrt{\gamma}$ so that

$$P_e = \int_0^\infty \text{erfc}(x) \sum_{i=1}^P \sum_{n=0}^{M-1} \pi_{ni} \left[1 - \exp\left(-\frac{x^2}{\bar{\gamma}_{ni}}\right) \right] \\ \cdot \sum_{k=0}^{M-1} \frac{\pi_{ki}}{\bar{\gamma}_{ki}} \exp\left(-\frac{x^2}{\bar{\gamma}_{ki}}\right) x dx \\ = \frac{1}{2} \sum_{i=1}^P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \frac{\pi_{ni}\pi_{ki}}{\bar{\gamma}_{ki}} \\ \cdot \left[\int_0^\infty 2x \text{erfc}(x) \exp\left(-\frac{x^2}{\bar{\gamma}_{ki}}\right) dx \right. \\ \left. - \int_0^\infty 2x \text{erfc}(x) \exp\left(-\frac{x^2}{\bar{\gamma}_{kni}}\right) dx \right] \quad (31)$$

with

$$\bar{\gamma}_{kni} = \frac{\bar{\gamma}_{ki}\bar{\gamma}_{ni}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni}} \quad (32)$$

If the two integrals in (31) are computed by parts, the expression of the mean BER obtained is given by

$$P_e = \frac{1}{2} \sum_{i=1}^P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_{ni}\pi_{ki} \\ \cdot \left[\left(1 - \sqrt{\frac{\bar{\gamma}_{ki}}{1 + \bar{\gamma}_{ki}}} \right) - \frac{\bar{\gamma}_{kni}}{\bar{\gamma}_{ki}} \left(1 - \sqrt{\frac{\bar{\gamma}_{kni}}{1 + \bar{\gamma}_{kni}}} \right) \right] \quad (33)$$

and after substituting (32) in (33), the final expression is

$$P_e = \frac{1}{2} \sum_{i=1}^P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_{ni}\pi_{ki} \\ \cdot \left[\frac{\bar{\gamma}_{ki}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni}} + \frac{\bar{\gamma}_{ni}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni}} \right. \\ \left. \cdot \sqrt{\frac{\bar{\gamma}_{ki}\bar{\gamma}_{ni}}{\bar{\gamma}_{ki} + \bar{\gamma}_{ni} + \bar{\gamma}_{ki}\bar{\gamma}_{ni}}} - \sqrt{\frac{\bar{\gamma}_{ki}}{1 + \bar{\gamma}_{ki}}} \right] \quad (34)$$

APPENDIX B

To simplify the computation of

$$P_e = \frac{1}{2} E[\text{erfc}(\sqrt{\gamma})] \\ = \frac{1}{2} \int_0^\infty \text{erfc}(\sqrt{\gamma}) \sum_{n=0}^{M-1} \pi_n \\ \cdot \left(\frac{\gamma}{\bar{\gamma}_n^2} - \frac{2}{\bar{\gamma}_n} \sum_{i \neq n} \frac{\bar{\gamma}_i}{\bar{\gamma}_n - \bar{\gamma}_i} \right) \exp\left(-\frac{\gamma}{\bar{\gamma}_n}\right) d\gamma \quad (35)$$

let us make the change of variable $x = \sqrt{\gamma}$ so that

$$\begin{aligned}
P_e &= \int_0^\infty \operatorname{erfc}(x) \sum_{n=0}^{M-1} \pi_n \left(\frac{x^3}{\bar{\gamma}_n^2} - \frac{2x}{\bar{\gamma}_n} \sum_{i \neq n} \frac{\bar{\gamma}_i}{\bar{\gamma}_n - \bar{\gamma}_i} \right) \\
&\quad \cdot \exp\left(-\frac{x^2}{\bar{\gamma}_n}\right) dx \\
&= \sum_{n=0}^{M-1} \pi_n \left[\frac{1}{\bar{\gamma}_n^2} \int_0^\infty x^3 \operatorname{erfc}(x) \exp\left(-\frac{x^2}{\bar{\gamma}_n}\right) dx \right. \\
&\quad \left. - \frac{2}{\bar{\gamma}_n} \sum_{i \neq n} \frac{\bar{\gamma}_i}{\bar{\gamma}_n - \bar{\gamma}_i} \int_0^\infty x \operatorname{erfc}(x) \right. \\
&\quad \left. \cdot \exp\left(-\frac{x^2}{\bar{\gamma}_n}\right) dx \right]. \tag{36}
\end{aligned}$$

It is convenient to compute the integrals in (36) by parts, so it is straightforward to obtain the expression of the mean BER

$$\begin{aligned}
P_e &= \sum_{n=0}^{M-1} \pi_n \left[\left(\frac{1 - \mu_n}{2} \right)^2 (2 + \mu_n) \right. \\
&\quad \left. - (1 - \mu_n) \sum_{i \neq n} \frac{\bar{\gamma}_i}{\bar{\gamma}_n - \bar{\gamma}_i} \right] \tag{37}
\end{aligned}$$

where

$$\mu_n = \sqrt{\frac{\bar{\gamma}_n}{1 + \bar{\gamma}_n}}. \tag{38}$$

APPENDIX C

When a Rake receiver is employed, the parameter $D(\lambda)$ can be expressed as [9, vol. II, p. 50]

$$D(\lambda) = E \left\{ \exp \left[- \sum_{n=0}^{M-1} \alpha_n^2 (2\lambda \sqrt{E_b} - \lambda^2 I) \right] \right\}. \tag{39}$$

Let us define

$$\lambda = s \frac{\sqrt{E_b}}{I} \tag{40}$$

and notice that the signal-to-interference ratio at the output of the Rake receiver is

$$\gamma_b = \sum_{n=0}^{M-1} \alpha_n^2 \frac{E_b}{I} \tag{41}$$

so (39) can be transformed in

$$D(s) = E \{ \exp[-\gamma_b(2s - s^2)] \}. \tag{42}$$

To compute this average, we need the expression of the pdf of γ_b given by (7), so that

$$\begin{aligned}
D(s) &= \int_0^\infty e^{-\gamma_b(2s-s^2)} \left\{ P \sum_{n=0}^{M-1} \pi_n \left[1 - \exp\left(-\frac{\gamma_b}{\bar{\gamma}_n}\right) \right] \right. \\
&\quad \left. \cdot \sum_{k=0}^{M-1} \frac{\pi_k}{\bar{\gamma}_k} \exp\left(-\frac{\gamma_b}{\bar{\gamma}_k}\right) \right\} d\gamma_b
\end{aligned}$$

$$= P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_n \pi_k \left[\frac{1}{1 + \bar{\gamma}_k(2s - s^2)} - \frac{\bar{\gamma}_n}{\bar{\gamma}_n + \bar{\gamma}_k + \bar{\gamma}_n \bar{\gamma}_k(2s - s^2)} \right]. \tag{43}$$

Then, minimizing the parameter $D(s)$ expressed in (43), the following expression is obtained:

$$\begin{aligned}
D &= \min_{s \geq 0} D(s) \\
&= P \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} \pi_n \pi_k \left[\frac{1}{1 + \bar{\gamma}_k} - \frac{\bar{\gamma}_n}{\bar{\gamma}_n + \bar{\gamma}_k + \bar{\gamma}_n \bar{\gamma}_k} \right]. \tag{44}
\end{aligned}$$

APPENDIX D

When MRC is selected as form of diversity, from (42) we have that

$$\begin{aligned}
D(s) &= \int_0^\infty e^{-\gamma_b(2s-s^2)} \left[\sum_{n=0}^{M-1} \right. \\
&\quad \left. \cdot \pi_n \left(\frac{\gamma_b}{\bar{\gamma}_n^2} - \frac{2}{\bar{\gamma}_n} \sum_{i \neq n} \frac{\bar{\gamma}_i}{\bar{\gamma}_n - \bar{\gamma}_i} \right) \exp\left(-\frac{\gamma_b}{\bar{\gamma}_k}\right) \right] d\gamma_b \\
&= \prod_{n=0}^{M-1} \left[\frac{1}{1 + 2\bar{\gamma}_n(2s - s^2)} \right]. \tag{45}
\end{aligned}$$

Therefore, the D parameter is given by

$$D = \min_{s \geq 0} D(s) = \prod_{n=0}^{M-1} \left(\frac{1}{1 + \bar{\gamma}_n} \right)^2. \tag{46}$$

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Pilar Díaz (M'94) was born in Barcelona, Spain, on November 29, 1967. She received the Engineer and Doctor Engineer degrees in telecommunication engineering from the Universitat Politècnica de Catalunya (UPC), Spain, in 1990 and 1994, respectively.

In 1990, she joined the Escola Tècnica Superior d'Enginyers de Telecomunicació de Barcelona, Spain, where she became an Assistant Professor in 1991 and an Associate Professor in 1995. She has been working in the field of digital radio communications with particular emphasis on personal, indoor, and mobile communications. Her main research interests lie in the area of radio multiple access and spread-spectrum systems, both FH and DS/CDMA systems. She participated in the RACE Program and Cost European Action, and at present, she is actively participating in the ACTS European Research Program.



Ramón Agustí (M'78) was born in Riba-roja d'Ebre, Spain, on August 15, 1951. He received the Engineer of Telecommunication degree from the Universidad Politècnica de Madrid, Spain, in 1973 and the Ph.D. degree from the Universitat Politècnica de Catalunya (UPC), Spain, in 1978.

In 1973, he joined the Escola Tècnica Superior d'Enginyers de Telecomunicació de Barcelona, Spain, where he became Full Professor in 1987. He has been working in the field of digital communications with particular emphasis on digital radio, both fixed radio relay and mobile communications. He has also been concerned with the performance analysis and development of frequency-hopped spread-spectrum systems. He participated in the COST 231 and RACE European research programs and currently is participating in the ACTS program. His research interests are in the area of mobile communications with special emphasis on CDMA systems and packet radio networks.